

## Atomistic mechanisms of moisture-induced fracture at copper-silica interfaces

Dandapani Vijayashankar, Hong Zhu, Saurabh Garg, Ranganath Teki, R. Ramprasad, Michael W. Lane, and Ganpati Ramanath

Citation: *Appl. Phys. Lett.* **99**, 133103 (2011); doi: 10.1063/1.3622304

View online: <https://doi.org/10.1063/1.3622304>

View Table of Contents: <http://aip.scitation.org/toc/apl/99/13>

Published by the [American Institute of Physics](#)

---

### Articles you may be interested in

[On the physics of moisture-induced cracking in metal-glass \(copper-silica\) interfaces](#)

*Journal of Applied Physics* **102**, 053516 (2007); 10.1063/1.2775998

---

**HIDEN**  
ANALYTICAL

## Instruments for Advanced Science

Contact Hiden Analytical for further details:

**W** [www.HidenAnalytical.com](http://www.HidenAnalytical.com)

**E** [info@hiden.co.uk](mailto:info@hiden.co.uk)

**CLICK TO VIEW** our product catalogue



#### Gas Analysis

- › dynamic measurement of reaction gas streams
- › catalysis and thermal analysis
- › molecular beam studies
- › dissolved species probes
- › fermentation, environmental and ecological studies



#### Surface Science

- › UHV TPD
- › SIMS
- › end point detection in ion beam etch
- › elemental imaging - surface mapping



#### Plasma Diagnostics

- › plasma source characterization
- › etch and deposition process reaction
- › kinetic studies
- › analysis of neutral and radical species



#### Vacuum Analysis

- › partial pressure measurement and control of process gases
- › reactive sputter process control
- › vacuum diagnostics
- › vacuum coating process monitoring

## Atomistic mechanisms of moisture-induced fracture at copper-silica interfaces

Dandapani Vijayashankar,<sup>1</sup> Hong Zhu,<sup>2</sup> Saurabh Garg,<sup>1</sup> Ranganath Teki,<sup>1</sup> R. Ramprasad,<sup>2</sup> Michael W. Lane,<sup>3</sup> and Ganpati Ramanath<sup>1,a)</sup>

<sup>1</sup>Materials Science and Engineering Department, Rensselaer Polytechnic Institute, Troy, New York 12180, USA

<sup>2</sup>Chemical, Materials and Biomolecular Engineering Department, University of Connecticut, Storrs, Connecticut 06269, USA

<sup>3</sup>Chemistry Department, Emory and Henry College, Emory, Virginia 24327

(Received 17 April 2011; accepted 9 July 2011; published online 26 September 2011)

Tailoring the chemo-mechanical properties of metal-dielectric interfaces is crucial for many applications including nanodevice wiring, packaging, composites, and catalysis. Here, we combine moisture-induced fracture tests, electron spectroscopy, and density functional theory calculations to reveal fracture toughness partitioning and atomistic delamination mechanisms at copper-silica interfaces. Copper plasticity is supported above a threshold work of adhesion and delamination occurs by moisture-induced Cu-O bond scission in Cu-O-Si bridges. These results provide insights into the effects of the nature of metal-oxygen bonding on moisture-induced delamination of metal-dielectric interfaces. © 2011 American Institute of Physics. [doi:10.1063/1.3622304]

Metal-ceramic interfaces are of key importance in diverse applications including nanoelectronics, sensors, communication devices, composites, and catalysis.<sup>1</sup> Heterointerfacial fracture toughness  $\Gamma_{FT}$  typically consists of the interfacial bond-breaking work of adhesion  $\gamma_a$  (Ref. 2) and plasticity  $\gamma_p$ , in the layers.<sup>3</sup> Plasticity is often a function of  $\gamma_a$ , which in turn is sensitive to the crack-tip chemical environment.<sup>3,4</sup> Unveiling the fracture mechanism and partitioning  $\Gamma_{FT}$  into  $\gamma_a$  and  $\gamma_p$  are crucial for tailoring the chemo-mechanical properties and stability of heterointerfaces for applications.

Although copper-silica interfaces are known to be susceptible to stress corrosion-cracking, e.g., in water, alcohols and amides,<sup>5,6</sup> the atomistic fracture mechanism is yet to be understood. Theoretical calculations<sup>7</sup> have shown that strong Cu-O bonds promote, and hydroxyl groups degrade, copper-silica interfacial adhesion. Oxygenated copper films exhibiting a 40% higher copper-silica interface toughness has been attributed to Cu-O-Si bridging.<sup>8</sup> Involvement of dissociative adsorption of reactive species at Cu-O-Si bridges in the fracture mechanism has also been hypothesized,<sup>5</sup> but is yet to be verified.

Here, we combine moisture-induced fracture tests, electron spectroscopy and density functional theory calculations to reveal the atomistic delamination mechanisms at copper-silica interfaces. We show that copper plasticity is supported above a threshold work of adhesion, and delamination occurs by moisture-induced Cu-O bond scission in Cu-O-Si bridges. These findings provide insights into the effects of the nature of metal-oxygen bonding on the delamination of metal-dielectric interfaces.

We sputter-deposited 50-nm-thick copper films followed by a 150-nm-thick Ta overlayer at a 7 mTorr Ar<sup>+</sup> plasma without vacuum break in a  $7 \times 10^{-7}$  Torr base pressure CVC sputter tool on Si(001) wafers capped with a 85-nm thick thermal silica layer. The Ta layer offsets the poor adhesion

between Cu and an epoxy used to obtain 50 mm  $\times$  5 mm rectangular beams of dummy-Si/epoxy/Ta/Cu/SiO<sub>2</sub>/Si(001) stacks for four point bend interfacial fracture tests as described in detail elsewhere.<sup>9,10</sup> We prepared stacks with Au/SiO<sub>2</sub> interfaces by the same method.

We conducted four-point-bend fracture tests at water activities between  $0.05 \leq a_{H_2O} \leq 0.8$  at  $T = 323$  K in a Cincinnati Sub-Zero PZ series chamber. The test structure beams were displaced at 10 nm/s in a high stiffness micromechanical system operated at a 43° phase angle.<sup>11</sup> The interfacial crack emanates from a notch scribed using a diamond saw on the Si wafer hosting the Cu film. The first plateau in the load-displacement curve<sup>11</sup> corresponds to a critical crack driving energy  $\Gamma_c$  at which the crack reaches and propagates along the weakest interface at the given displacement rate. Arresting the displacement at the plateau relaxes the load monotonically at a continually decreasing crack velocity  $v$ . As  $v \rightarrow 0$ , the crack driving energy  $\Gamma$  diminishes to the equilibrium fracture toughness<sup>11</sup>  $\Gamma_{FT}$ . Since  $\Gamma_{FT}$  is extracted from the steep part of the  $v$ - $\Gamma$  curves,  $\Gamma_{FT}$  connotes reaction-kinetics-limited delamination at the crack tip.

The  $v$ - $\Gamma$  plots obtained from structures with copper-silica and gold-silica interfaces (Figure 1) at different  $a_{H_2O}$  indicate that  $\Gamma_{FT}^{Cu}$  is sensitive to  $a_{H_2O}$  for copper-silica interfaces [see Fig. 2(a)]. Decreasing  $a_{H_2O}$  from 0.8 to 0.05 results in a nearly five-fold increase in  $\Gamma_{FT}^{Cu}$  from 1.1 to 5.4 J/m<sup>2</sup> for copper-silica interfaces. This value is comparable to 1.9 J/m<sup>2</sup> reported for Cu-SiO<sub>x</sub>N<sub>y</sub> interfaces<sup>12</sup> for 20%–40% humidity. In contrast,  $\Gamma_{FT}^{Au} \approx 0.5 \pm 0.1$  J/m<sup>2</sup> is significantly lower and independent of  $a_{H_2O}$ . These differences can be understood in terms of the vastly different oxidation potentials of copper and gold. While  $\Gamma_{FT}^{Cu}$  is dependent on Cu-O-Si bond formation and its susceptibility to water,<sup>5,8</sup> the low  $\Gamma_{FT}^{Au}$  stems from the lack of thermodynamic driving force for Au-O bond formation<sup>13</sup> at room temperature, thereby precluding further moisture-induced weakening. Fitting  $v$ - $\Gamma$  characteristics of the Au/silica interface to a reaction rate kinetics model for water-induced fracture in orthosilicates<sup>14,15</sup> yields a crack propagation activation

<sup>a)</sup>Author to whom correspondence should be addressed. Electronic mail: Ramanath@rpi.edu.

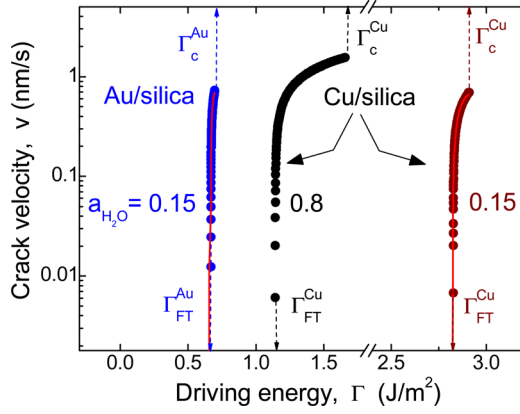


FIG. 1. (Color online) Crack velocity vs. driving energy ( $v$ - $\Gamma$ ) curves as a function of  $a_{\text{H}_2\text{O}}$  at 323 K for copper-silica and gold-silica interfaces. The solid lines represent the reaction rate kinetics model fits for  $a_{\text{H}_2\text{O}} = 0.15$ .

energy of  $0.193 \pm 0.002$  eV that is lower than that for Si-O-Si hydrolysis,<sup>14</sup> suggesting that Au-O-Si hydrolysis is kinetically favored. The extracted interfacial bond density  $N_i^{\text{Au}} = 0.1 \times 10^{15}$  atoms/cm<sup>2</sup> is in reasonable agreement with  $1.4$ – $1.9 \times 10^{15}$  atoms/cm<sup>2</sup> oxygen coverage on silica surfaces.<sup>16</sup>

For copper-silica interfaces, we observe two distinct regimes about  $a_{\text{H}_2\text{O}} \sim 0.2$ . In both regions,  $\Gamma_{\text{FT}}^{\text{Cu}}$  increases linearly with decreasing  $\log a_{\text{H}_2\text{O}}$ , but the slope of toughness increase  $|\frac{d\Gamma_{\text{FT}}^{\text{Cu}}}{d\log a_{\text{H}_2\text{O}}}|$  is four-fold higher for  $a_{\text{H}_2\text{O}} < 0.2$  than that for  $a_{\text{H}_2\text{O}} > 0.2$ . We note that plotting  $a_{\text{H}_2\text{O}}$  on a log scale connotes the water chemical potential  $|\text{RT} \log a_{\text{H}_2\text{O}}|$ , where  $R$  is the gas constant. For  $a_{\text{H}_2\text{O}} \sim 0.2$ ,  $\Gamma_{\text{FT}}^{\text{Cu}} \sim 2.1$  J/m<sup>2</sup>, in good agreement with  $\gamma_a = 2.2$  J/m<sup>2</sup> for copper-silica interfaces.<sup>16</sup> For  $a_{\text{H}_2\text{O}} > 0.2$ ,  $\Gamma_{\text{FT}}^{\text{Cu}} < 2.1$  J/m<sup>2</sup> due to water-induced Cu-O-Si weakening and/or fissure. Thus, for  $a_{\text{H}_2\text{O}} > 0.2$ , the mechanical energy supplied is used solely for interfacial bond breaking, i.e.,  $\Gamma_{\text{FT}} = \gamma_a$ . Since  $\gamma_a \propto N_i \text{RT} \log a_{\text{H}_2\text{O}}$  at equilibrium ( $v \rightarrow 0$ ), we obtain  $N_i^{\text{Cu}} = 8.7 \times 10^{15}$  atoms/cm<sup>2</sup>, which is within about an order of magnitude of the oxygen coverage on silica<sup>16</sup> and  $N_i^{\text{Cu}} = 0.4 \times 10^{15}$  atoms/cm<sup>2</sup> obtained by fitting the  $v$ - $\Gamma$  data to a reaction-rate kinetics model. This fit also yields a crack-propagation activation energy of  $0.204 \pm 0.002$  eV/bond for Cu-O-Si hydrolysis, implying that Cu-O-Si bond breakage is kinetically favored over siloxane bridge scission.

For  $a_{\text{H}_2\text{O}} < 0.2$ , copper-silica interfaces exhibit  $2.1 < \Gamma_{\text{FT}}^{\text{Cu}} < 5.4$  J/m<sup>2</sup> which are significantly higher than  $\gamma_a$ . This result and the higher toughness increase rate for  $a_{\text{H}_2\text{O}} < 0.2$  indicate an additional energy dissipation mechanism, identified to be copper plasticity.<sup>4</sup> The linear increase in  $\Gamma_{\text{FT}}^{\text{Cu}}$  with decreasing  $\log a_{\text{H}_2\text{O}}$  for  $a_{\text{H}_2\text{O}} < 0.2$  is consistent with increasing plasticity because the plastic zone size is expected to linearly increase<sup>4</sup> with  $\gamma_a$ . Thus, at low water activities  $a_{\text{H}_2\text{O}} < 0.2$  the Cu-O-Si interfacial bonds are strong enough to support plastic deformation in copper, leading to significant contributions from both  $\gamma_p$  and  $\gamma_a$  to  $\Gamma_{\text{FT}}^{\text{Cu}}$ . We extract  $\gamma_p$  from the difference between  $\Gamma_{\text{FT}}^{\text{Cu}}$  and  $\gamma_a$  by extrapolating the linear fit of  $\gamma_a$  vs.  $|\log a_{\text{H}_2\text{O}}|$  plot to the desired  $a_{\text{H}_2\text{O}}$  in the low-humidity region. This extrapolation is valid since  $\gamma_a$  is dependent solely on  $a_{\text{H}_2\text{O}}$ . Thus,  $\gamma_p$  can be described as a function of  $\gamma_a$  [see Fig. 2(b)]:  $\gamma_p = \tau(\gamma_a - \gamma_0)$ , where  $\gamma_a = \gamma_0$  at yield

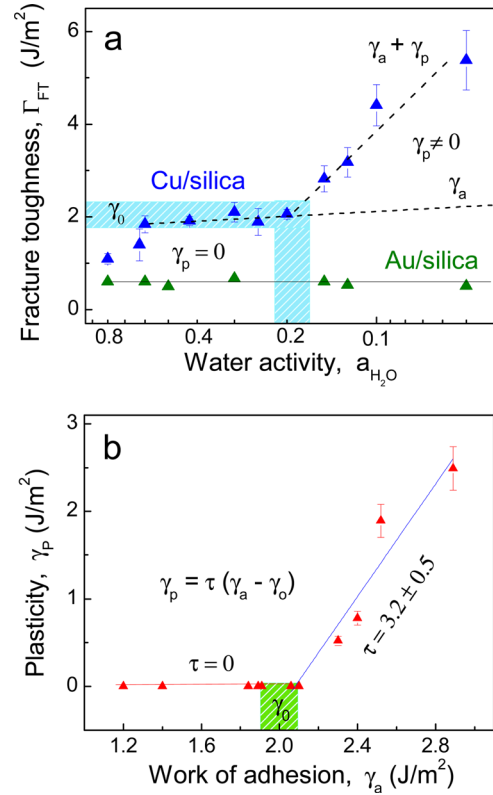


FIG. 2. (Color online) (a) Fracture toughness  $\Gamma_{\text{FT}}$  plotted as a function of  $a_{\text{H}_2\text{O}}$  at 323 K for copper-silica and gold-silica interfaces. In this plot,  $a_{\text{H}_2\text{O}}$  is on a log scale, (b) Copper plastic energy  $\gamma_p$  vs interfacial work of adhesion  $\gamma_a$  at 323 K.

point.<sup>17</sup> For  $\gamma_a < \gamma_0$ ,  $\gamma_p = \tau = 0$ , but  $\gamma_p$  increases linearly with  $\gamma_a$  with  $\tau \sim 3$  for  $\gamma_a > \gamma_0$ , consistent with  $0.2 < \tau < 8$  predicted by analytical models for heterointerfaces.<sup>2</sup>

Fracture surface analysis by X-ray photoelectron spectroscopy reveals that delamination occurs through bond-breaking at the metal-dielectric interface. The Cu fracture surfaces show strong Cu  $2p_{3/2}$  and  $2p_{1/2}$  sub-bands at 932.7 eV and 953 eV, respectively [see Fig. 3(a)], these peak intensities are very low in spectra acquired from the silica fracture surfaces. The Si  $2p$  band centered at 103.3 eV is observed only on the silica fracture surface and is undetectable on the Cu fracture surface.

In order to understand the bond-breaking mechanisms at the crack tip, we consider the energetics of hydrolysis of Cu-O and Si-O bonds, expressed by  $\text{Cu-O} + \text{H-O-H} \rightarrow \text{Cu-OH} + \text{OH}$  with  $\Delta G_{\text{hydrolysis}}^{\text{Cu-O}} = 3.3$  eV and  $\text{Si-O} + \text{H-O-H} \rightarrow \text{Si-OH} + \text{OH}$  with  $\Delta G_{\text{hydrolysis}}^{\text{Si-O}} = 9.2$  eV. Since  $\Delta G_{\text{hydrolysis}} > 0$  for both reactions, calculated using the relevant bond free energies<sup>15,18</sup> at 323 K, the hydrolysis of neither Cu-O nor Si-O bonds is thermodynamically favored. However, the mechanical driving force in our experiments can offset this constraint. The free energy magnitudes of the reactions indicate that the Cu-O bonds need a lower mechanical driving force to break via hydrolysis than Si-O bonds. This inference is supported by the results of density functional theory (DFT) calculations carried out to assess the impact of moisture on the copper-silica interface strength.

Our DFT calculations used the VASP code<sup>19</sup> with the PW91 generalized gradient approximation<sup>20</sup> and projector-augmented wave approach.<sup>21,22</sup> Assuming that interfacial

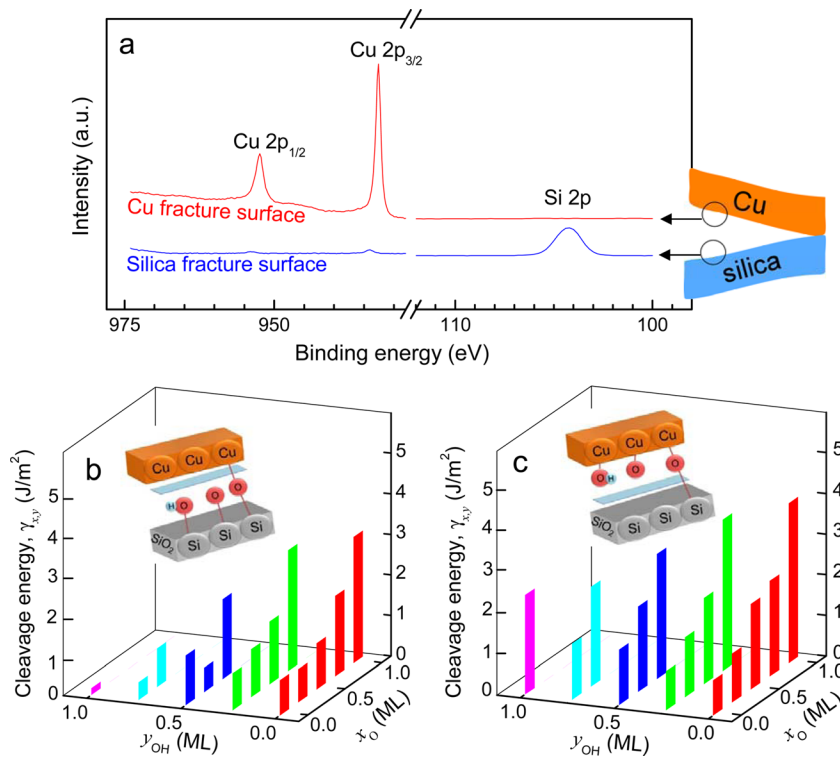


FIG. 3. (Color online) (a) Core-level Cu 2p sub-band and Si 2p sub-band from a Cu/SiO<sub>2</sub> interface, measured by x-ray photoelectron spectroscopy at  $a_{\text{H}_2\text{O}} = 0.85$  and  $T = 323$  K. Cleavage energy  $\gamma_{xy}$  plotted as a function of interfacial O and OH coverages for (b) breaking Cu-O/Cu-OH bonds and (c) breaking Si-O/Si-OH bonds. The schematic sketches indicate the location of Cu-O-Si bridge scission.

moisture produces hydroxyl species, we considered copper-silica interfaces with different O and OH coverages,  $x_O$  and  $y_{OH}$ , respectively, for cleavage at Cu-O or Si-O bonds [see Figs. 3(b) and 3(c)]. We note that cleaving *interfacial* Cu-O bonds results in Si-OH and Si-O passivated surfaces, while breaking *interfacial* Si-O bonds forms Cu-OH and Cu-O species at the interface. These reaction pathways and energetics of hydrolysis of *interfacial* Cu-O or Si-O bonds are different from that of *stand-alone* Cu-O and Si-O bonds described above. The cleavage energy  $\gamma_{xy}$  can be computed for various values of  $x_O$  and  $y_{OH}$  using  $\gamma_{xy} = E_{\text{Cu}} + E_{\text{SiO}_2} - E_{xy}$ , where  $E_{\text{Cu}}$ ,  $E_{\text{SiO}_2}$ , and  $E_{xy}$  are the DFT energies for the cleaved fragments of Cu and SiO<sub>2</sub>, and their heterointerface, respectively. We find that  $\gamma_{xy}$  increases with  $x_O$ , as expected [Figs. 3(b) and 3(c)], pointing to the importance of oxygen-bridged bonds at copper-silica interfaces. Cu-O scission requires a lower  $\gamma_{xy}$  than for Si-O bond fissure for the  $x_O$  and  $y_{OH}$  ranges explored. However, the energy difference between Cu-O and Si-O cleavage given by  $\Delta\gamma_{xy}$ , which is  $<0.4$  J/m<sup>2</sup> at low water content, e.g.,  $y_{OH} < 0.25$ , and more pronounced at  $\Delta\gamma_{xy} \sim 1.5$  J/m<sup>2</sup> at higher moisture levels, e.g.,  $y_{OH} > 0.75$ . Thus, the Cu-O bond is the weaker link especially at higher moisture contents, supporting the claim that copper-silica interfaces fracture via water-induced scission of Cu-O-Si bridges at the Cu-O bonds.

In conclusion, the work of adhesion at copper-silica interfaces is determined by moisture-induced scission of Cu-O bonds in Cu-O-Si bridges. Above a threshold work of adhesion, the interfacial bonds support copper plasticity. Our findings provide atomistic insights into environmental effects of delamination of metal-dielectric interfaces, and are relevant to many applications ranging from microelectronics to biological implants.

We gratefully acknowledge funding from the NSF through DMR 0519081, CMMI 1100933/926, and ECCS 1002282/301 awards, and a NRI-NIST grant through the Index Center at the University at Albany.

- <sup>1</sup>M. Ruhle, A. H. Heuer, A. G. Evans, and M. F. Ashby, *Acta Metall. Mater.* **40**, S1 (1992).
- <sup>2</sup>M. Lane, R. H. Dauskardt, N. Krishna, and I. Hashim, *J. Mater. Res.* **15**, 203 (2000).
- <sup>3</sup>J. W. Hutchinson and Z. Suo, *Adv. App. Mech.* **29**, 63, 1992.
- <sup>4</sup>A. Jain, B. Singh, S. Garg, N. Ravishankar, M. Lane, and G. Ramanath, *Phys. Rev. B* **83**, 035412 (2011).
- <sup>5</sup>J. C. Card, R. M. Cannon, E. Saiz, A. P. Tomsia, and R. O. Ritchie, *J. Appl. Phys.* **102**, 053516 (2007).
- <sup>6</sup>J. J. Kruzic, J. M. McNaney, R. M. Cannon, and R. O. Ritchie, *Mech. Mater.* **36**, 57 (2004).
- <sup>7</sup>K. Nagao, J. B. Neaton, and N. W. Ashcroft, *Phys. Rev. B* **68**, 125403 (2003).
- <sup>8</sup>M. Z. Pang and S. P. Baker, *J. Mater. Res.* **20**, 2420 (2005).
- <sup>9</sup>D. D. Gandhi, M. Lane, Y. Zhou, A. P. Singh, S. Nayak, U. Tisch, M. Eizenberg, and G. Ramanath, *Nature* **447**, 299 (2007).
- <sup>10</sup>P. G. Ganesan, A. P. Singh, and G. Ramanath, *Appl. Phys. Lett.* **85**, 579 (2004).
- <sup>11</sup>Q. Ma, *J. Mater. Res.* **12**, 840 (1997).
- <sup>12</sup>M. P. Hughey, D. J. Morris, R. F. Cook, S. P. Bozeman, B. L. Kelly, S. L. N. Chakravarty, D. P. Harkens, and L. C. Stearns, *Eng. Fract. Mech.* **71**, 245 (2004).
- <sup>13</sup>G. C. Bond, *Catal. Today* **72**, 5 (2002).
- <sup>14</sup>B. R. Lawn, *Fracture of Brittle Solids* (Cambridge University Press, UK, 1993).
- <sup>15</sup>R. F. Cook and E. G. Liniger, *J. Am. Ceram. Soc.* **76**, 1096 (1993).
- <sup>16</sup>A. Bhatnagar, M. J. Hoffman, and R. H. Dauskardt, *J. Am. Ceram. Soc.* **83**, 585 (2000).
- <sup>17</sup>V. Tvergaard and J. W. Hutchinson, *Philos. Mag. A* **70**, 641 (1994).
- <sup>18</sup>M. D. Allendorf, C. F. Melius, P. Ho, and M. R. Zachariah, *J. Phys. Chem.* **99**, 15285 (1995).
- <sup>19</sup>G. Kresse and J. Furthmuller, *Phys. Rev. B* **54**, 11169 (1996).
- <sup>20</sup>J. P. Perdew, J. A. Chevary, S. H. Vosko, K. A. Jackson, M. R. Pederson, D. J. Singh, and C. Fiolhais, *Phys. Rev. B* **46**, 6671 (1992).
- <sup>21</sup>P. E. Blochl, *Phys. Rev. B* **50**, 17953 (1994).
- <sup>22</sup>G. Kresse and D. Joubert, *Phys. Rev. B* **59**, 1758 (1999).